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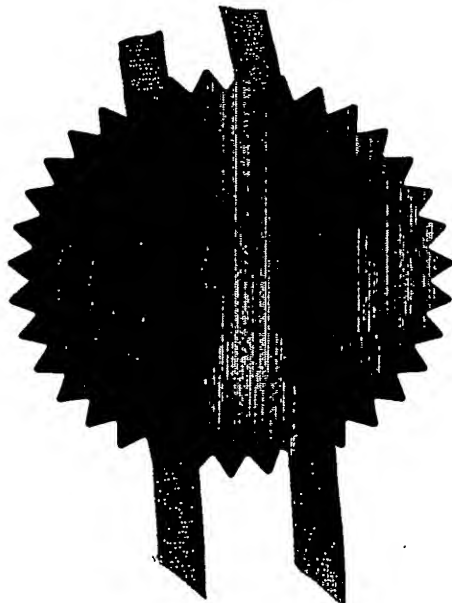
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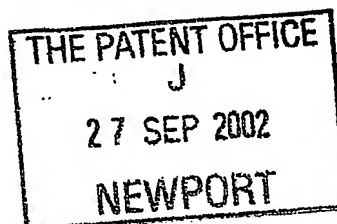


1/77

27SEP02 E751435-1 C27915
P01/7700 0.00-0222421.0

Request for grant of a patent

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1. Your reference

HKR-UTL

2. Patent application number

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0222421.0

3. Full name, address and postcode of the or of each applicant (underline all surnames)

HENRY KEVIN RATCLIFF
6 PARK COURT,
ALEXANDRA DRIVE
LIVERPOOL, MERSEYSIDE
2832640004 L17-8TA

Patents ADP number (if you know it)

If the applicant is a corporate body, give the country/state of its incorporation

4. Title of the invention

ADVANCED ULTRASONIC PROCESSOR

5. Name of your agent (if you have one)

"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)

~~MY ADDRESS AS GIVEN~~
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see
5/177

Graham Jones + Company
77 Beaconsfield Road
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6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or of each of these earlier applications and (if you know it) the or each application number

Country

Priority application number
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Date of filing
(day / month / year)

7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application

Number of earlier application

GB 0121681.1

Date of filing
(day / month / year)
8/09/2001

TITLE: ULTRASONIC GENERATOR

8. Is a statement of inventorship and of right to grant of a patent required in support of this request? (Answer 'Yes' if:

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See note (d))

Patents Form 1/77

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Description

14

Claim(s)

NONE AT THIS STAGE

Abstract

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Priority documents

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Statement of inventorship and right to grant of a patent (Patents Form 7/77)

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Request for substantive examination (Patents Form 10/77)

Any other documents (please specify)

11. I/We request the grant of a patent on the basis of this application.

Signature

Date

Henry Kevin Ratchett

26/09/02

12. Name and daytime telephone number of person to contact in the United Kingdom

HENRY KEVIN RATCHETT
TEL/FAX: 0151- 727-1370

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DESCRIPTION

ADVANCED ULTRASONIC PROCESSOR

The present invention is concerned with improving performance and efficiency of continuous-throughput ultrasonic processors.

An important application of the invention concerns processing of drill cuttings in the oil industry, but the invention is also applicable in other fields including processing of mineral ores, land remediation and water treatment.

In drilling for oil, it is common practice to feed a drilling fluid, typically a mineral oil-based mud, to the cutting head. The cuttings resulting from the drilling have in the past been left to disperse on the seabed, but this is recognised as a potential environmental hazard.

It is known to collect this mixture and to process it. In the case of sub-sea drilling the cuttings and mud are together driven to the surface for collection. The cuttings-solids, which may contain toxic substances, are separated from the mud in one of several ways.

Known methods include the use of screen shakers, ball mills, hydro cyclones and centrifuges. The mud, which is valuable is cleaned and reused. The cuttings themselves must be disposed of and this may be done by re-injection thereof into a disposal well. It is known to do this by first mixing the cuttings with seawater to form slurry, and then processing the cuttings to reduce their particle size to enable re-injection of the cuttings in the disposal well. Alternatively, the processed cuttings may be returned to shore for treatment.

It is known to utilize ultrasound in processing of the drill cuttings. The mixture collected from the well is exposed to ultrasound in a processor having a continuous

throughput and the violent, highly localized pressure and temperature fluctuations created by cavitation associated with the ultrasonic waves de-agglomerate the mixture. Large particles are broken down and the mixture is then suitable for disposal.

A known ultrasonic processor for use in this context is disclosed in published European patent application EP 841982 and its US equivalent 6079508. It has a tubular metal body through which a continuous flow of material is passed. Ultrasonic vibrations are applied to the tube's exterior by means of a set piezoelectric transducers bolted to the tube's curved outer surface, being seated upon respective saddles, whose inner faces are curved to match the tube and through which the ultrasonic waves are transmitted to the tube wall and through it to the material to be processed. Using this type of arrangement it has proven necessary to connect several individual processors in series in processing drill cuttings. It is considered that this type of arrangement is inefficient in its use of the wave energy provided by the transducers.

On oilrigs, space and energy are both at a premium. An object of the present invention is to provide an especially energy efficient ultrasonic processor in converting high-frequency electrical energy from the generator or power supply into sonic energy in the process chamber with a substantial reduction in size of the processor footprint, as compared with the known ultrasonic processor.

Known ultrasonic processors use either a multiplicity of low intensity, non-resonant transducers bonded to the outer surface of a pipe with average power density less than 1 W cm^{-2} , or single, high power density ($40\text{-}60 \text{ W cm}^{-2}$) transducers (of the type used for ultrasonic welding) which may be welded to a pipe. (Power density is here defined as electrical power input to a processing system or transducer divided by its radiating surface area). It is considered that both types of arrangement are inefficient. In

the former case, the sonic energy may not penetrate more than 2 cm into the fast-flowing laden liquid. In the latter, high sonic power density focused on a small section of pipe may be expected to generate significant heat at that point. It may also be expected that a substantial proportion of the ultrasonic energy supplied by the transducer will be dissipated as heat as it flows along the pipe wall, more especially if the pipe is made of steel, which has poor acoustic properties. And with narrow pipe diameter, and consequent high flow velocity, residence time of the material in the ultrasonic field will be short.

A further objective of the invention is to increase both acoustic efficiency and performance of the ultrasonic processor by an arrangement in which a closely-packed group of high-intensity transducers is bonded to a wall so as to develop a uniform, high power density ultrasonic field across its surface with negligible acoustic loss therein.

In accordance with the present invention, there is an ultrasonic processor comprising a processor chamber having an input and an output communicating with the chamber's interior for throughput of material to be processed, and a bank of ultrasonic transducers coupled to a wall of the processor chamber for transmitting ultrasonic waves to the material in the chamber; wherein the input is displaced from the output along a connecting wall in a direction perpendicular to the chamber wall to which the bank of transducers is coupled.

Various advantages derive from the present invention.

The inventor has recognised that it is desirable in order to improve processor efficiency to achieve a stable standing ultrasonic wave pattern in the processor chamber and therefore maximum cavitation for a given energy input.

A stable standing wave inside the liquid is the best condition for cavitation, as the pressure variations in the medium are then at a maximum. Thus, minimum energy is required for cavitation or, vice versa, maximum intensity occurs for a given power input.

The inventor has further recognised that the tubular type of processor referred to above does not achieve a well defined standing wave pattern (corresponding to strong resonant behaviour). The tubular shape of the processor means that the laterally directed sound waves, if reflected at all from the processor's internal walls, form a complicated pattern and not a well defined sonic standing wave.

Moreover, if a standing wave were formed in the known tubular type of processor, there would be a risk of some material failing to be processed at all. The cavitation, which is in large part responsible for processing, occurs in zones of rarefaction produced by the ultrasonic waves. The result of establishing a stable standing wave pattern would be to localize these zones. In the known tubular processor, wave propagation is essentially across the processor tube, so a stable standing wave would correspond to a situation in which some pattern of compression and rarefaction of the wave pattern existed across the tube's width. Since the direction of the flow of material to be processed is along the length of the tube (i.e. essentially perpendicular to the direction of wave propagation) a proportion of the material passing along a zone of compression of the wave pattern, may not be subject to the necessary cavitation action.

In a processor constructed according to the present invention, material passes from the input in the sidewall at the lower end of the processor chamber, to the output in the sidewall at the upper end of the chamber. And, therefore, as the material moves along the direction of wave propagation it must pass through compression and rarefaction zones of any standing wave pattern and so must pass through regions of cavitation and thereby be processed in accordance with designated number of wave fronts and relative attenuation.

It can be expected that, in the simple case of a generally planar wave front, the wave front is generally parallel to the wall, which is acted on by the transducers

and hence, the standing wave pattern is formed along a direction generally perpendicular to this wall.

In a particularly preferred embodiment of the present invention, the displacement of the input from the output along the sidewall is greater than the wavelength of ultrasound in the processor chamber at the driven frequency of the transducer.

In a further preferred embodiment of the present invention, the wall upon which the ultrasonic transducers are mounted is at least substantially flat,

The processor chamber has a second wall opposed to the wall on which the ultrasonic transducers are mounted across the interior of the processing chamber and at least substantially parallel thereto.

The arrangement is well suited for creating a sonic standing wave in material in the processing chamber. Waves induced by the transducer bank acting upon one of the walls are reflected from the opposed wall and, if the drive frequency of the transducer bank is appropriately chosen, the resulting travelling waves, propagating in opposite directions, constructively interfere to form a sonic standing wave. This principle is very well known to those skilled in the art.

It is especially preferred that the two walls are separated by a distance which is substantially an integral or half integral multiple of wavelength of ultrasound in the processor chamber at the driven frequency of the transducer. This condition maximizes constructive interference of the outgoing and reflected waves.

Power density in the mixture being processed may in a further preferred embodiment of the present invention, be increased by providing respective ultrasonic transducers acting on both of the opposed walls. To ensure constructive interference, provision could in such an embodiment be made for adjusting the phase of one bank of transducers relative to the other.

It is a further preferred that the ultrasonic transducer modules be coupled to the chamber wall through a wave-guide.

The wave-guide performs a function analogous to impedance matching in an electronic circuit, minimizing reflection at the coupling between the transducers and the processor chamber

The present invention makes it possible to use a processor chamber of large cross section as compared with the known tubular processors referred to above. Preferably, the cross section of the processor chamber (measured perpendicular to the flow direction through it) is substantially greater than 125 cm^2 (the cross section of a known tubular processor). In the currently preferred embodiment, the processor chamber has a cross section of substantially 1000 cm^2 .

Clearly, for a given throughput of material being processed, the rate of flow is inversely proportional to the chamber's cross-section. A low rate of flow, achievable by means of the large cross section made possible by the present invention is beneficial in establishing efficient ultrasound action. This is because disturbances of the mixture being processed are found to reduce the ultrasonic power density in the mixture. In a processor having a relatively high flow velocities, such as the tubular processor referred to above, it is considered unlikely that a stable and powerful standing wave could be achieved. The slower flowing material in a large cross-section chamber is less prone to disturbance, enables stable standing waves to be established and maintained under load conditions, and increases the interval of time the mixture being processed is resident in the processing chamber, and thus is more conducive to efficient ultrasonic action.

A specific embodiment of the present invention will now be described by way of example only, with reference to the accompanying drawings, in which: Fig 1 is a vertical sectional view of an ultrasonic processor embodying the present invention;

Fig 2 is a view of the same processor from beneath;

Fig 3 is a side, sectional view of an arrangement of transducer module and wave-guide used in the processor.

Fig 4 illustrates the standing wave in the processor;

Fig 5 is a view from one side of a drill cuttings processing system utilizing two processors of the type illustrated in Figs.1 to 4; and

Fig 6 is a view from the side of an alternative construction of a processor according to the present invention.

The ultrasonic processor 10 illustrated in Figs 1 to 4 comprises a chamber 12 formed of metal and having a sidewall 14 which is in the illustrated embodiment circular in plan (although other shapes could be used) and which is closed at its upper and lower ends by end walls 16 and 18 respectively.

The end walls are opposed across the interior 20 of the chamber, and are in the illustrated embodiment flat and mutually parallel.

Coupled to the lower wall 18 is a bank of ultrasonic transducers 22. The layout of individual transducers 22 is shown in Fig, 2, each being indicated by a circle for the sake of representational convenience, and positioned for minimum spacing one from the other.

In the current invention, the arrangement of transducers on the end wall 18 is intended to raise acoustic efficiency by minimising loss of energy due to destructive interaction between adjacent transducers. To this end, the transducers may be positioned at nodes or null points calculated from the known transverse speed of sound in the metal comprising the lower end wall or plate 18, and to include rectangular wave-guides with their sides within 5 mm of each other.

In this arrangement, which is unconventional, a batch of high-intensity ultrasonic transducers is bonded to a metal plate in such a manner that the plate itself becomes a resonant element at the driven frequency of the electrical generator. The device, so

constructed, would appear to be a single entity, and to perform as if it were a high-power transducer of large cross section.

The transducer assembly 18, thus described, will generally be acoustically decoupled from the chamber sidewall 14 and straightforwardly removable for replacement. Furthermore, the assembly may also find use in high power density ultrasonic applications not yet considered.

The wave-guides used in the invention, as with horns in ultrasonic welding applications, can be of various shapes, invert of the above. Conical wave-guides with square cross section at the lower end 18 may be designed to achieve the objective of uniform pre-determined power density at the wall surface to which the transducers are attached.

Wave-guides may be designed as velocity transformers to step down the power density at the radiating face of a high-intensity transducer to a still high, but more usable value. e.g. a cone ratio of 1:4 between cross section of the radiating face of the 200 W transducer module 22 and that of the wave-guide 24 will provide a uniform power density of 5 W cm⁻² at the radiating face of the wall 18. .

The transducer of Fig 3, may be driven by an ultrasonic switching generator operating directly from the rectified 50/60 Hz line or main power, with the high frequency sinusoidal drive to the transducer being developed by the output inductance of the generator in electrical resonance with the capacitance of the piezoelectric elements 26/28. The operating frequency of the system is the mechanical resonant frequency of the wave-guide. Alumina ceramic washers 36/37 provide electrical isolation from the 50/60 Hz line.

The transducer may also be driven from a generator with transformer output, in which case the operating frequency will be determined by the overall length of the transducer elements including wave-guide 24 and the transducer module 22.

In the arrangement illustrated in Fig 3, each transducer module 22 is bolted to a respective rod wave-guide 24, a washer 37 being interposed therebetween and the contacting faces of the transducer module. The washer and the wave-guide being flat and compressed together by the bolt 25 in order that ultrasonic waves can be efficiently passed from the transducer module 22 to the wave-guide 24.

Each wave-guide is attached, in the illustrated embodiment, by brazing, to the outer face of the lower end wall 18. Hence, ultrasonic vibrations in the wave-guide can be transmitted to the lower end wall 18 and, through the wall, to the contents of the processor. The metal wave-guide brazed to the end wall 18 provides a robust mounting for the transducer module 22. The transducer module itself, being simply bolted to the wave-guide, is straightforwardly removable for replacement.

The wave-guide allows the ultrasonic waves to be transmitted to the wall 18 efficiently, minimising power reflected to the transducer, which otherwise reduces efficiency.

The length of the currently preferred wave-guide is half a wavelength of sound, at the processor's operating frequency, in the wave-guide material. Some variation in adjustment of this operating frequency may be present in practice, but since the velocity of sound in the wave guide 24 (which is made of titanium in the present embodiment) is several times greater than the velocity of sound in the material being processed, such variations in frequency, and also variations in the properties of the materials being processed, will not greatly affect the match between the rod wave guide 24 and its load. (An aluminium wave-guide with a suitable fixing means may be used instead of titanium)

The effect of a wave-guide half a wavelength long is to place the interface between the wave-guide and the processor wall at a node in the standing wave pattern: i.e. to minimise variations in the wave amplitude at this interface. The general principle is known, e.g. in context of ultrasonic welding in which it is understood that the material

to be welded will at nodes of minimum wave motion accept power at vibratory frequency of a welding horn with minimum loss.

The transducer module 22 is of piezoelectric type in the illustrated embodiment. Between the piezoelectric elements 26,28 is sandwiched a first electrode 30 connected to the high side of the oscillator circuit 32. Second electrodes 34,36 are provided in the outer surfaces of the respective piezoelectric elements and connected to the low side of the oscillator circuit. The well-known effect of the oscillating electric fields produced by means of the electrodes is to cause a periodic change in the length of the piezoelectric elements. Due to inertia, contributed mainly by a back mass 38, the transducer module consequently causes the wave-guide 24 to vibrate. The bank of transducers 22 is driven in phase. The back mass 38 is at the transducer arrangement's outermost end, the head of the bolt 25 bearing upon the back mass through a compression washer 27.

Electrical isolation for the transducer is provided by means of isolating washers 35,37. In the illustrated embodiment, these isolating washers are formed as alumina rings. An upper one of the washers 35 is interposed between the uppermost electrode 36 and the back mass; the lower washer 37 is interposed between the lowermost electrode 34 and the wave-guide 24. The bolt 25 is also provided with an insulating sleeve. In this way, it becomes possible to dispense with the isolating transformers in the electrical supply, a significant source of heat. This is especially important when constructing a fully enclosed processor, as required in the oil industry, where heat output must be minimised in order to achieve an acceptable operating temperature, and Zone 1 certification.

The isolating washers 35,37 sandwich, and are chemically bonded to the electrodes 34,36 and in this way a robust transducer module is constructed.

The material (in this case alumina oxide) of the isolating washers 35,37 is chosen to give enhanced wave transmission. Alumina oxide has an acoustic velocity significantly higher than that of aluminium or titanium, and so provides efficient acoustic coupling.

The result is a highly efficient transducer producing little waste heat. In the illustrated embodiment, the transducer is driven at between 20 and 80 kHz, and more typically 20 and 40 kHz.

Turning back to Fig 1, throughput of material is provided for by means of an input pipe 40 close to the bottom of the processor chamber 12 and an output pipe 42 close to its top, both communicating with the interior 20 of the chamber. While the input 40 and output 42 are both radially directed, and are laterally separated, it will be apparent that they are also separated along a sidewall 14 in direction perpendicular to the wall 18 (i.e. parallel to the chamber's axis, in this current embodiment). The direction of the flow of material in the chamber 12 must have an axial component – i.e. the material must move along a direction from the bottom of the chamber to the top as indicated by arrow 43 – although there must be a radial component in the flow direction, and clearly the velocity and precise direction of the flow must vary from one point to another within the chamber. The speed of this flow is low (in comparison with prior art ultrasonic tubular processors) due to the large cross section of the processor chamber 12, which has a diameter of approximately 36 cm. Residence time of the material in the processor chamber is correspondingly long (25 seconds is not untypical)

Fig 4 illustrates in highly schematic form the behaviour of ultrasonic waves in the processor chamber 12. The transducer module 22, wave-guide 24, and end walls 16,18 are all labelled as in earlier drawings. The drawing 44 shows a wave outgoing from the wall 18 as a solid line and a wave 46 which has been reflected from the upper wall 16 as a dotted line. As the skilled person will readily appreciate, the superposition of the outgoing and reflected waves 44,46 can, if the wavelength is appropriately chosen with respect to

the path length of the waves, be a sonic standing wave. The currently preferred embodiment uses a frequency in the region of 20 kHz to produce a standing wave pattern having 6 wavelengths in the processor chamber.

Because the direction of the flow of material through the processor chamber has a component which is along the direction of propagation of the outgoing and reflected waves 44,46, the material flowing through the processor must pass through alternate zones of compression and rarefaction of the standing wave pattern. This progression through the chamber 12 in the direction 43 ensures that the material is ultrasonically processed by cavitation action in each of several rarefaction zones therein.

Additionally, large particles in the material being processed are believed to tend to remain, due to their large mass, at the lower end of the processor chamber until broken down by the action of the ultrasound, thereby increasing residence time of these particles and so improving particle size reduction.

Certain prior art processors intended for processing large liquid loads employ individual high-intensity transducers as probes, the heads of which project into a chamber to activate the liquid mixture contained therein. The transducers themselves are secured to the chamber wall by nodal flanges, and are thus acoustically isolated from the chamber wall itself. (e.g. WO 00/54095; J59087026).

This type of ultrasonic processor, in which probe transducers are used to activate liquid in a vessel, is considered inefficient. Thermal and acoustic coupling of probes to the volume of liquid in a chamber is poor, with consequent thermal problems

Another prior art unit (W0 01/17672) intended for processing drill cuttings is similar to the above referenced tubular processor: The ultrasonic wave is applied perpendicular to the flow of slurry in the processor. This unit features an inner cylinder, which in conjunction with the outer wall forms a narrow, annular processing chamber. Apparently,

this tubular processor uses low intensity (non resonant) transducers, widely spaced as shown in Figs 1, 2, thus, providing low power density in the outer tube (driven) wall. Acoustic losses in this wall, made of stainless steel, and the inner chamber, with its helical steel ribbon, may be expected to be high.

This tubular processor (though avoiding possible disruption of the ultrasonic field by laminar flow in the wide diameter inner tube) also appears to be inefficient in using the ultrasonic energy supplied by the transducers.

The liquid capacity of the above tubular processors is about 12 litres. For a typical drill cuttings application, with liquid capacity flow rate of 2 litres per second (1 barrel per minute), the processors may be said to have a residence time of about 6 seconds. Four such processors connected in series may be needed to provide adequate ultrasonic processing time. But such an arrangement, especially if the processors are connected in serpentine formation, may have the disadvantage, when drilling stops, of sedimentation blocking the lower coupling pipes.

In accordance with the present invention, the processor chamber will be about 50 cm deep and have a liquid capacity of 50 litres. Since there is no fundamental limitation on the dimensions of the chamber in cross section, processors can be custom built to specification.

Also, if necessary, the processors of the current invention can be connected in series with the advantage that sediment deposited on the surface of a wall to which transducers are attached, is likely to be cleared automatically by ultrasonic action when the processor is switched on.

The processor 10 can be utilized in a processing system such as the arrangement 100 illustrated in Fig 5. In fact this system has two such processors mounted and, for safety purposes enclosed one above the other in a frame 102 by means of respective acoustic isolation clamps 104,106. The system has an input 108 to the lowermost processor 10'' whose output is led via a transfer conduit 110 to the uppermost processor 10' and through this to the system output 112.

The input 108, output 112 and transfer conduit 110 are each formed as pipes of substantially 5cm diameter.

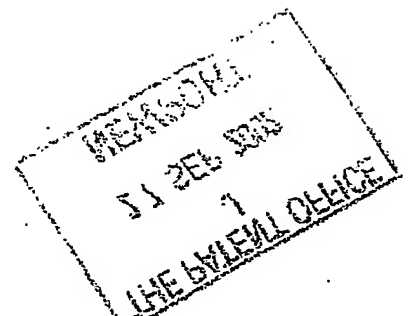
Series connection of the two processors increases the time for which the material is exposed to ultrasound and hence the effectiveness of the system in reducing particle size.

Drive circuits suitable for driving the transducers are known to the skilled person and are not described herein, but reference is directed in this connection to the inventor's own U.S. Patents 4588917 and U.S. 4554477. Both describe circuits having "frequency sweep" (periodic variation of drive frequency) and "autofollow" (automatic adjustment of drive frequency) and both or either of these features may be used in the present invention.

The processor of the current invention is expected to have a drill cuttings throughput rate of the order of 2 tonne per kW hour and electrical to acoustic energy-conversion efficiency close to 95 %.

Fig 6 illustrates alternative configurations of input and output for the processor chamber. The illustrated ultrasonic processor 100''' has a lower end wall 118 upon which are mounted the transducers 122. The processor chamber 112 is again cylindrical, lower end wall 118 and upper wall 116 being circular. Input 140 is in this embodiment axially (i.e. upwardly) directed passing through the end wall 118. The output may likewise be axial, passing through the upper end wall as indicated in the phantom at 142. It may alternatively be radial taken through the chamber's sidewall as indicated at 142'.

While the illustrated embodiments use processor chambers of circular section other shapes, including rectangular section, may be used.



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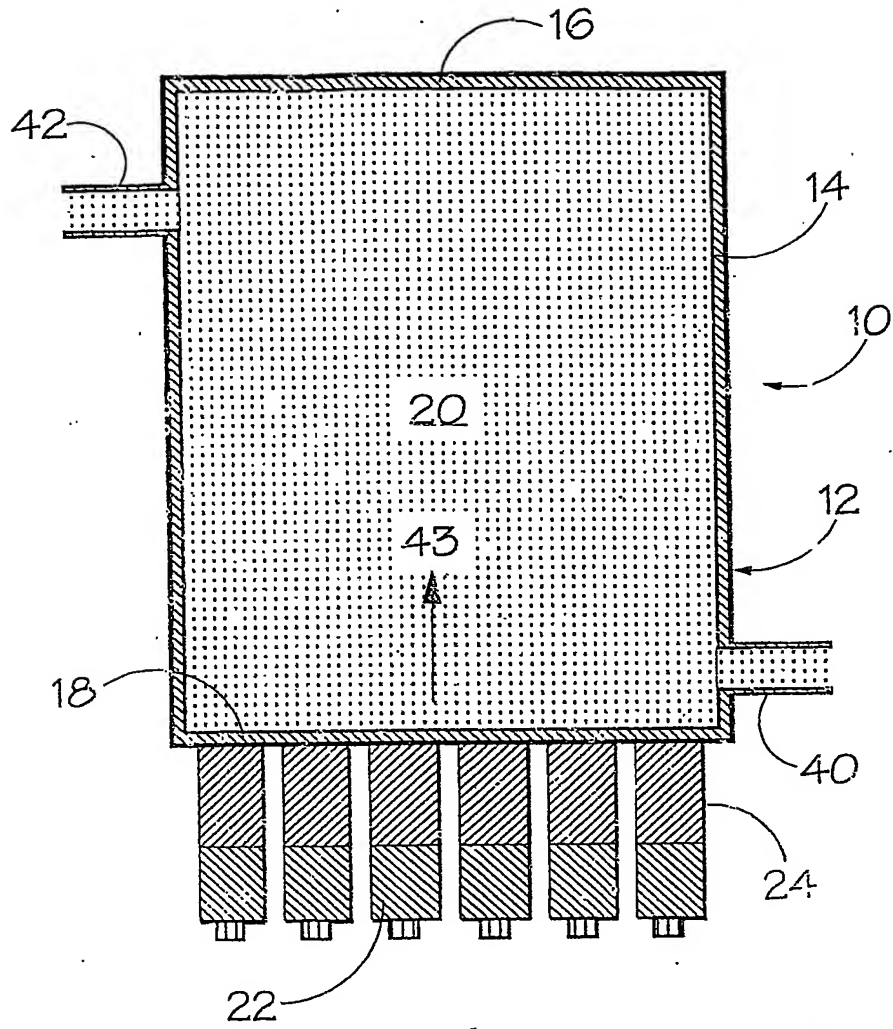


FIG. 1.

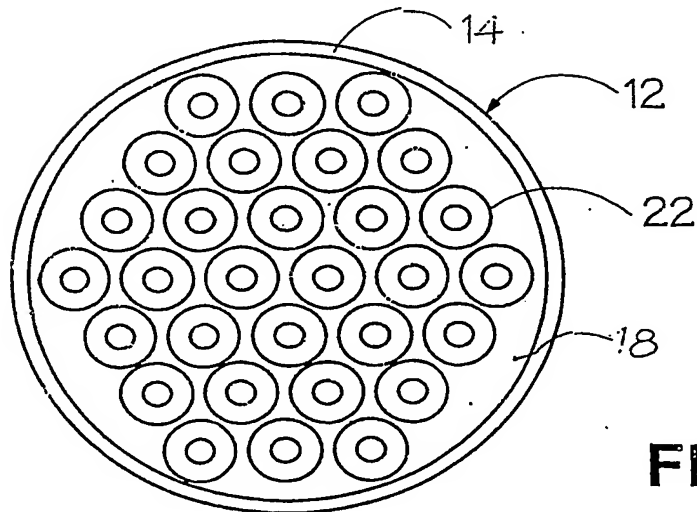
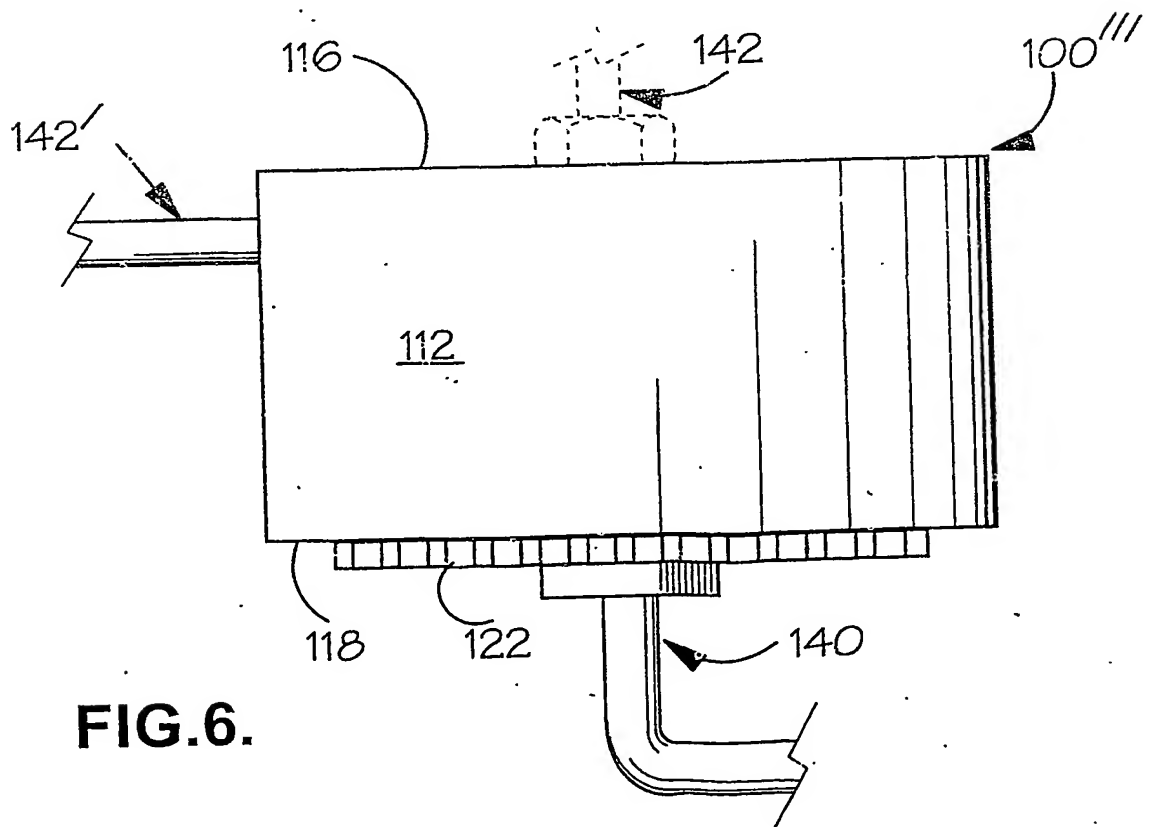
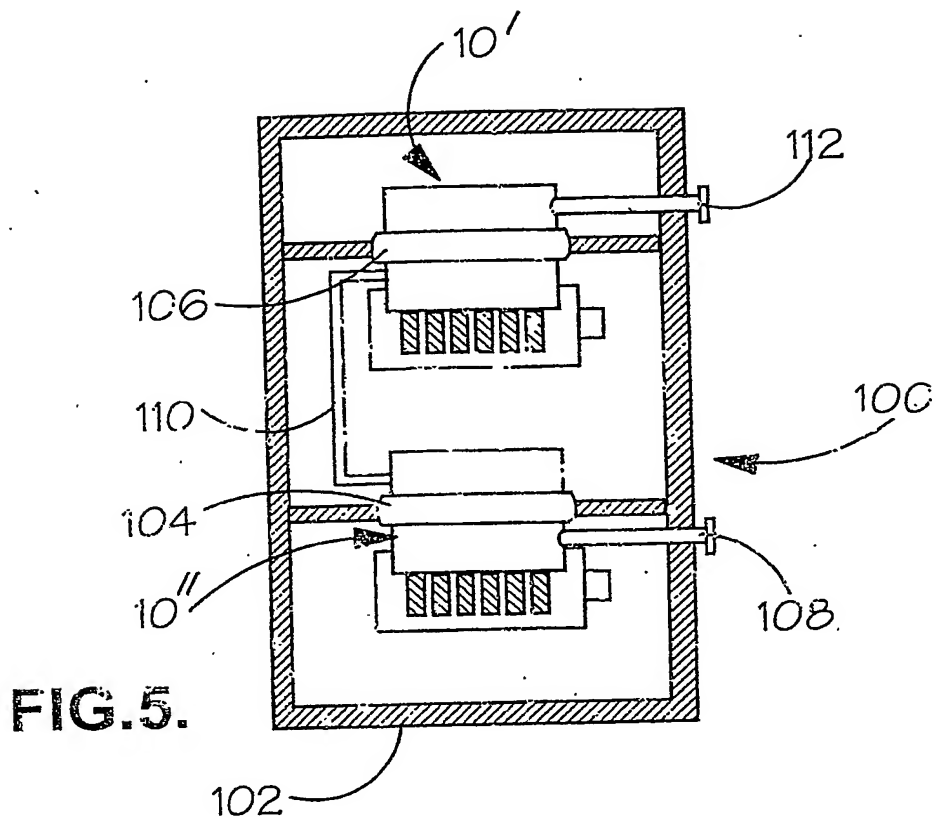


FIG. 2.





PCT Application

GB0304185



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